

# Heat Transfer Final Exam

## (Model Correction)

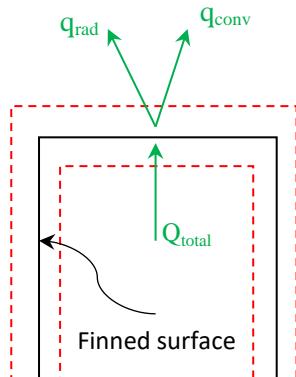
### Problem n° 01 (08 points):

1) The energy balance on the finned surface in terms of:  $Q_{total}$ ,  $q_{conv}$  and  $q_{rad}$ :

Taking a control surface from the finned surface:

$$E_{in} + E_g - E_{out} = E_{st} \quad (\text{Where: } E_g = 0, \text{ and } E_{st} = 0)$$

Give  $E_{in} = E_{out}$  then,  $Q_{total} = q_{conv} + q_{rad}$  1



2) The total surface area ( $A_{s, total}$ ) for heat transfer :

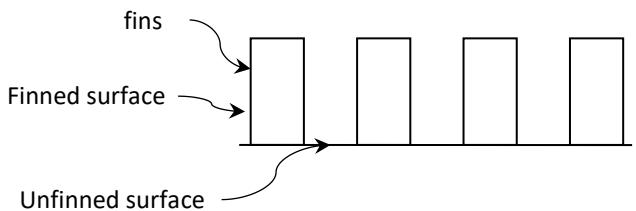
$$A_{s, total} = A_{s, finned} + A_{s, unfinned} \quad \text{0.5}$$

$$A_{s, finned} = 7 \times (2 \times (5 \times 100)) + (2 \times (2 \times 5)) + (2 \times 100) \quad \text{0.5}$$

$$A_{s, finned} = 85.4 \text{ cm}^2 = 0.0085 \text{ m}^2 \quad \text{0.5}$$

$$A_{s, unfinned} = (10 \times 6.2) - (7 \times 0.2 \times 10)$$

$$A_{s, unfinned} = 48 \text{ cm}^2 = 0.0048 \text{ m}^2 \quad \text{0.5}$$



Give:  $A_{s, total} = 0.00133 \text{ m}^2$  1

3) The radiation heat transfer rate ( $q_{rad}$ ):

We have:  $q_{rad} = \varepsilon \cdot A_{s, total} \cdot \sigma \cdot (T_s^4 - T_{surr}^4)$  0.5

Then,  $q_{rad} = 0.9 \times 0.0133 \times 5.67 \times 10^{-8} ((60 + 273)^4 - (25 + 273)^4)$ , give :  $q_{rad} \approx 3 \text{ W}$  0.5

4) The heat transfer coefficient ( $h$ )

The convection heat transfer coefficient can be determined from *Newton's law of cooling* relation for a finned surface.

$$q_{conv} = \eta \times h \times A_s \times (T_\infty - T_s) \rightarrow h = \frac{q_{conv}}{\eta \times A_s \times (T_\infty - T_s)} \rightarrow h = \frac{q_{conv}}{0.90 \times 0.0133 \times (60 - 25)} \quad \text{0.5}$$

Where:  $q_{conv} = Q_{total} - q_{rad} = 12 \text{ W} - 3 \text{ W} = 9 \text{ W}$  0.5

Then  $h = \frac{9}{0.90 \times 0.0133 \times (60 - 25)}$  give:  $h \approx 21.50 \text{ (}\frac{W}{m^2} \cdot ^\circ C\text{)}$  0.5

5) The minimum free-stream velocity ( $U_{min}$ ) the fan needs to supply to avoid overheating:

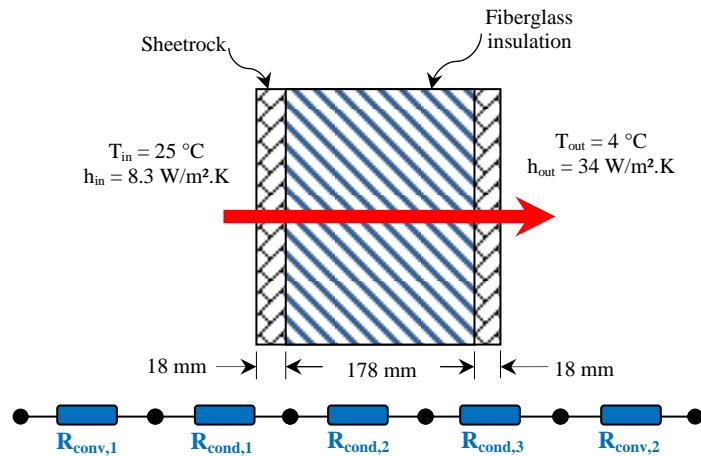
Starting from heat transfer coefficient, *Nusselt number*, *Reynolds number* and finally free-stream velocity will be determined. We assume the flow is laminar over the entire finned surface of the transformer.

$$Nu = \frac{hL}{k} = \frac{21.5 \times 0.1}{0.02681} = 80.20 \quad \text{With, } Nu = 0.664 Re_L^{0.5} Pr^{1/3} \rightarrow Re_L = \frac{Nu^2}{0.664^2 \times Pr^2} = \frac{(80.20)^2}{(0.664)^2 \times (0.7248)^{2/3}} \approx 1.8 \times 10^4 \quad \text{0.5}$$

Then,  $Re_L = \frac{U_{min} L}{v} \rightarrow U_{min} = \frac{Re_L \times v}{L} = \frac{1.8 \times 10^4 \times 1.726 \times 10^{-5}}{0.1} \rightarrow U_{min} = 3.11 \text{ m/s}$  0.5  
0.5

**Problem n° 02 (04 points):**

1) Draw the thermal resistance circuit for this wall :



1

2) Determine the thermal resistance of the wall :

$$R_{wall} = R_{conv,1} + R_{cond,1} + R_{cond,2} + R_{cond,3} + R_{conv,2}$$

$$R_{wall} = \frac{1}{h_{in} \cdot A} + \frac{L_{sheetrock}}{k_{sheetrock} \cdot A} + \frac{L_{fiberglass}}{k_{fiberglass} \cdot A} + \frac{L_{sheetrock}}{k_{sheetrock} \cdot A} + \frac{1}{h_{out} \cdot A}$$

1

$$R_{wall} = \frac{1}{8.3 \times (5 \times 3)} + \frac{0.018}{0.15 \times (5 \times 3)} + \frac{0.178}{0.02 \times (5 \times 3)} + \frac{0.018}{0.15 \times (5 \times 3)} + \frac{1}{h_{out} \times (5 \times 3)}$$

$$R_{wall} = 0.008 + 0.008 + 0.5933 + 0.008 + 0.002 \rightarrow R_{wall} \approx 0.6193 (\text{°C/W})$$

1

3) Calculate the heat transfer rate through the wall :

$$q = \frac{T_{\infty,in} - T_{\infty,out}}{R_{wall}} = \frac{25 - 4}{0.6193} \rightarrow q = 33.91 (\text{W})$$

1

**Problem n° 03 (08 points):**

1) The variation of temperature  $\frac{T(x) - T(\infty)}{T(b) - T(\infty)}$  along the spoon :

Assuming that the heat transfer from the tip of the spoon is negligible, then, the variation of temperature will be given from Table 1, by:

$$\frac{T(x) - T(\infty)}{T(b) - T(\infty)} = \frac{\cosh m(L-x)}{\cosh mL}$$

2

(Equation 01)

2) Determine the temperature difference ( $\Delta T = T_b - T_{tip}$ ) across the exposed surface of the spoon :

Calculating  $T_{tip}$  means that:  $x = L = 7 \text{ in.}$

Substituting in (Equation 01),

$$\frac{T(L) - T(\infty)}{T(b) - T(\infty)} = \frac{\cosh m(L-L)}{\cosh mL} \rightarrow T_{tip} = \left( \frac{\cosh m(L-L)}{\cosh mL} \right) \times (T(b) - T(\infty)) + T(\infty)$$

1

$$m = \sqrt{\frac{hP}{kA_c}} = \sqrt{\frac{3 \times 2 \times (\frac{0.5+0.08}{12})}{8.7 \times (\frac{0.5 \times 0.08}{12})}} \rightarrow m = 10 \text{ ft}^{-1} \quad (\text{Inches to feet: } 1 \text{ ft} = 12 \text{ in})$$

$$T_{tip} = \left( \frac{\cosh(0)}{\cosh(10 \times \frac{7}{12})} \right) \times (200 - 75) + 75 = \left( \frac{1}{\cosh(5.83)} \right) \times (125) + 75 = \left( \frac{1}{170.18} \right) \times (125) + 75$$

$\cosh(5.83) = 170.18$  (Using **Table 2**).

$$T_{tip} = 75.73 \text{ }^{\circ}\text{F} \rightarrow \Delta T = T_b - T_{tip} = 200 - 75.73 = 124.27 \text{ }^{\circ}\text{F}$$

### 3) Determine the fin heat transfer rate ( $q_f$ ):

From Table 1:  $q_f = M \cdot \tanh(mL)$

$$\text{Where: } M = \sqrt{hPkA_c} \theta_b = \sqrt{3 \times 2 \left( \frac{0.5+0.08}{12} \right) \times 8.7 \times \left( \frac{0.5 \times 0.08}{12} \right) \times 125} \rightarrow M = 11.4$$

$$\tanh(mL) = \tanh \left( 10 \times \frac{7}{12} \right) = \tanh(5.83) = 0.999$$

$$q_f = 11.38 \text{ Btu/h}$$

1

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1

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